Evaluation procedure for blowing machine monitoring and predicting bearing SKFNU6322 failure by power spectral density

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Abstract

This work shows the results of the comparative study of characteristic frequencies in terms of Power Spectral Density (PSD) or RMS generated by a blower unit and the SKFNU322 bearing. Data is collected following ISO 10816, using Emonitor software and with speed values in RMS to avoid high and low frequency signal masking. Bearing failure is the main cause of operational shutdown in industrial sites. The difficulty of prediction is the type of breakage and the high number of variables involved. Monitoring and analysing all the variables of the SKFNU322 bearing and those of machine operation for 15 years allowed to develop a new predictive maintenance protocol. This method makes it possible to reduce from 6 control points to one, and to determine which of the 42 variables is the most incidental in the correct operation, so equipment performance and efficiency is improved, contributing to increased economic profitability. The tests were carried out on a 500 kW unit of power and It was shown that the rotation of the equipment itself caused the most generating variable of vibrational energy.

1. Introduction

Bearing failure is one of the most important causes of industrial equipment shutdown, in fact it is estimated that 40% of shutdowns are generated by bearings [28, 42]. Bearing failure is caused by many factors, such as lubrication, loads, handling failures, lack of preventive maintenance, among others [10, 34, 39].

ISO 10816-3 establishes that there are four stages of breakage, which are caused by unbalance, or misalignment [24, 32, 8]. Determining the stage is one of the main objectives of predictive maintenance and of industries in general, which are looking for this new technology to reduce the problem of production stoppages and the cost associated to them [4, 36]. Finding the breakage moment is the main objective, but the breakage type in the form of a ski curve makes this very difficult, because the transition from the third to the fourth stage takes place in a brief period of time involving corrective actions [18, 27]. Another problem is the number of fault types [22].

New non-invasive techniques, such as acoustic study, are trying to improve predictive maintenance [21, 23], but involve environmental problems. The approach by spectral analysis of the vibrations is the most widespread technique, but it requires several control points and daily monitoring, resulting in a large cost in terms of time and personnel [20]. Other approaches experiment with vector support machines (SVM) and Wavelet signal processing [1, 5].

Current studies determine the type of defect in the laboratory. The problem arises when it is analysed under real working conditions [9, 12, 13]. In order to validate the method, it is necessary to have very large control samples, which allow to discriminate external factors. Therefore, this research evaluates equipment monitoring over a 15-year period.

Although there is some background of similar studies to the one done here, none of them are applied to equipment of such a large size and power as used in this research, and in no case, those studies have been extended over such a long period of time. Thus, some research found have been applied in a small blowing machines for bottles [17, 37] evaluating the software used, and those carried out by [15, 38] in wind turbines, in which the data acquisition has been developed for less than three years.
2. Materials and methods

2.1. Equipment under study

It has been studied an air blower and the bearing SKFNU322, which supports the mechanical drive shaft between the blades and the motor. The driving system is a motor, model Framesize 400, 3190 kg and 1.9 x 0.9 metres. All this can be seen in Figure 1.

The blade system measures 2.075 meters in diameter and the connection between the two is made by a 0.095-metre diameter and 3.9-metres-long shaft. This equipment belongs to Atlantic Copper company.

Many studies on bearing vibration analysis have been carried out, since operational safety and efficiency, together with environmental protection, is one of the challenges of the world’s industry (McFadden and Smith 1984). Therefore, efforts are being made to meet this need through spectral vibration analysis [7, 14].

The dynamic state of movement and the actual operating conditions are the major milestones in laboratory studies. They analyse bearing failures [25, 40], but their approximations are not valid for real operating conditions.

Mechanical vibration is a set of impulses caused by hitting moving elements on coinciding areas. These energy effects under constant operating conditions generate stable frequency disturbances, which can be determined and discriminated according to the element that generates them [11]. Each bearing is made up of a cage, balls and tracks, and the impact between them generates different periodic waves, which have their own spectral range [6, 38].

The fault frequency of the components of bearing SKFNU322 is defined according to the contact points [19]. The service life of different bearing components is determined by the amplitude of a specific disturbance. The existing types and the mathematical expressions that define them are the following:

- The movement of rotation of the balls or rollers around their axis is what defines the frequency of rotation of each of them (Eq. 1):

  $$ BSF = 0.5 \times N \times \left( \frac{D}{d} \right) \times \left[ 1 - \left( \frac{d}{D} \right)^2 \right] $$  

- To determine the frequency of the ball defect, the so-called rotational frequency will be used, that is, twice the frequency of rotation of the balls or rollers (BSF), produced by the ball hit with both races (external and internal) at every turn (Eq. 2):

  $$ 2BSF = N \times \left( \frac{D}{d} \right) \times \left[ 1 - \left( \frac{d}{D} \right)^2 \right] $$

- The defect frequency of the ball support or rotation body (FTF) can be determined with the equation (3):

  $$ FTF = 0.5 \times N \times \left[ 1 - \left( \frac{d}{D} \right)^2 \right] $$

- The defect frequency produced in the ball passage or internal race (BPIR) and the defect frequency produced in the outer race or ball passage (BPOR) can be calculated with the expressions (4) and (5) respectively:

  $$ BPIR = 0.5 \times N \times \left[ 1 - \left( \frac{d}{D} \right)^2 \right] $$

  $$ BPOR = 0.5 \times N \times \left[ 1 - \left( \frac{d}{D} \right)^2 \right] $$

Where:
- $N$ is the angular speed of the axis in revolutions per second (rpm),
- $D$ is the average bearing diameter (inches),
- $d$ is the diameter of the rolling circumference of the balls or rollers (inches) and
- $n$ is the number of rollers or balls forming the bearing.

The blade frequency ($F_{pa}$) is the frequency generated by the blade passage and can be determined by the equipment rotational speed (RPM) and the blades number ($Na$) by using the equation (6):

$$ F_{pa} = Na \times \left[ \frac{\text{RPM}}{60} \right] $$

SKFNU322 bearing consists of 5 characteristic elements or frequencies, which are BSF, FTF, BPIR and BPOR, respectively. Another very important variable is $2BSF$, which is generated by the second harmonic of the balls [30].

The equipment uses the SKFNU322 bearing as a support for the power transmission shaft, between the motor and the blades. Table 1 shows the fundamental characteristics of the bearing.

<table>
<thead>
<tr>
<th>Basic dynamic load (C)</th>
<th>C 530 kN</th>
</tr>
</thead>
<tbody>
<tr>
<td>Basic static load (C0)</td>
<td>C0 540 kN</td>
</tr>
<tr>
<td>Fatigue limit load (Pu)</td>
<td>Pu 61 kN</td>
</tr>
<tr>
<td>Reference speed</td>
<td>3000 r/min</td>
</tr>
<tr>
<td>Speed limit</td>
<td>3400 r/min</td>
</tr>
<tr>
<td>Calculation factor (kr)</td>
<td>0.15</td>
</tr>
<tr>
<td>Geometric characteristics</td>
<td>d = 110 mm; D = 240 mm; B = 50 mm; d1 ≈ 200 mm; F = 143 mm; r1,2,3,4 min. 3 mm</td>
</tr>
</tbody>
</table>

They have been followed the guidelines of the ISO 10816.3 standard [43], to obtain the frequency spectra of the SKFNU322 bearing variables and the equipment fundamentals such as the blades and SPEED. The frequencies can be seen in the table below (Table 2).
Table 2. Characteristic frequencies of the bearing under study (Hz)

<table>
<thead>
<tr>
<th>Characteristic frequencies</th>
<th>Frequencies (Hz)</th>
</tr>
</thead>
<tbody>
<tr>
<td>FTF</td>
<td>601.96</td>
</tr>
<tr>
<td>BSF</td>
<td>3735.4</td>
</tr>
<tr>
<td>2BSF</td>
<td>7470.9</td>
</tr>
<tr>
<td>BPOR</td>
<td>8425.9</td>
</tr>
<tr>
<td>BPIR</td>
<td>12434.0</td>
</tr>
<tr>
<td>SPEED</td>
<td>1490.0</td>
</tr>
<tr>
<td>BLADES</td>
<td>13410.0</td>
</tr>
</tbody>
</table>

\[ X(f) = \frac{1}{\Delta T} \int_{-\infty}^{\infty} x(t) e^{-j2\pi ft} dt \]  

(7)

The improvement of the Fast Fourier Transform (FFT) allows to avoid signal masking or aliasing, in signals of small amplitude. The PSD or Power Spectral Density (e.g. applied in [26] and [33]), is the energy that has each characteristic frequency, this follows the mathematical expression below (Eq. 8):

\[ PSD(x(i)) = (1/T) \sum (x(i))^2 \Delta T \]  

(8)

The sum \( x(i) \) for \( \Delta T \) is the mean power of the interval. One way of estimating this energy is to limit the integration interval. It has been used a window based on the sample. This window is determined by the period o gram and allows to analyse hidden frequencies, avoiding signal masking [35].

The Hilbert HT transform (Hilbert Transform) studies the signal envelope. It achieves an improved PSD, making it easier to sample signals at low frequencies [31].

The method follows the procedure of transforming two functions \( s(t) \) and \( 1/(\pi t) \) into a third one, see the following mathematical expression (Eq. 9):

\[ \bar{x}(t) = \frac{1}{\delta} \int_{-\infty}^{\infty} x(u) \frac{1}{t-u} du \]  

(9)

The amplification of the signal envelope, for low frequency vibrations, provides improvements and disadvantages such as sensitivity to noise [29]. This was solved by the Wavelet Transform (WT), which provides information on signal processing such as time and frequency [41].

2.3. Data acquisition and processing

The study covers a period of 15 years, using Entel IRD and Odyssey Emonitor software for data acquisition and analysis. The measurement equipment has 16 channels with a nominal voltage of 24 V and 3.6 mA current.

The investigation was carried out on a 500 kW of power blow- ing machine with 3 m blades in a real operating conditions (constant regime) for 15 years and it was made by accredited technicians according to standard 18436-2, this fact makes this study unique in its category.

There are 4 filters used through a multiplexer, which generates acceleration, velocity and displacement signals. The accelerometer used has a sensitivity level of 100 mV/g., with a frequency range of 10000 Hz. The analogue-digital converter captures up to 51.2 kHz, with a resolution of 16 bit.

Monitoring is done through a magnetized anchor with quick release, which allows to reach faults with a frequency and sensitivity range between 0-300 Hz. A window of 3200 lines is used, with a range of 60000 to 300000 lines, depending on whether it is for speed or acceleration. The resolution of the Hanning window will be between 18 and 194 CPM, depending on the type of variable analysed (speed or acceleration).

According to the ISO 10816 standard, there are four levels of functional risk. For an equipment with flexible shaft, with power over 300 kW and speed of 1500 rpm, there would be an operating level that ranges from 0.18 to 11 RMS (mm/s), and its critical value is 7.1 RMS (mm/s), where corrective maintenance must be applied.

The ISO 10816 Standard, used for the diagnosis of vibration functionality in industrial equipment, determines that the evaluation should be done by the spectral level based on speed, as opposed to the use of acceleration or displacement, which only act properly at high or low frequency, respectively.

Integration considers the vibration signals produced at low frequency, acting to a lesser extent on those of high frequency. This is due to the proportional invertibility of the speed \( V(f) \) as a function of frequency \( f \), see the following expression (Eq. 10):

\[ V(f) = \frac{c_1 A(f)}{f} \]  

(10)

The \( D(f) \) shift is also affected by the frequency in an exponential way (Eq. 11):

\[ D(f) = \frac{c_2 A(f)}{f^2} \]  

(11)

where \( A(f) \) is the acceleration of frequency \( f \) and \( C_1 \) and \( C_2 \) are constants.

The equipment has 2 sampling points for data acquisition, these are called POS3 and POS4. In each of them, data are collected in the three space coordinates, identified as POS3H, POS3V and POS3A for the third position and the horizontal, vertical and axial axes, respectively. The monitoring of point 4 follows the same rule.

According to the indications of the standard 10816-3, there are three maximum levels that dictate the correct operation of the equipment. For this analysis, a total of 617 shots are obtained for each of the two positions and the three coordinated axes, resulting in a total of 3702 data. This data discriminates the variable, the position and the axis that are most decisive and influential in the operation of the equipment.

As a summary, Figure 2 includes a diagram with the procedure used.

3. Results and discussion

In the first instance, the characteristic frequencies of the SKFNU322 bearing in positions 3, 4 and their respective Cartesian axis are analysed. Within each position, the most critical axis is evaluated and compared with the other measurement position.

After the analysis of each frequency separately, they are all compared in their most sensitive positions to determine three fundamental elements, which would be the most harmful variable for the machine, its position and its axis.

Once the most sensitive variable of the bearing has been identified, it is related to the characteristic frequencies of the SPEED and Blades bearing in their most decisive control positions.

The analysis of the FTF frequency, generated by the bearing cage, is obtained by calculating the sum of values of the entire spectrum, at each of the control points. It is also done with the mean and the maximum or peak value, all in RMS.

For accumulated values and peak at position 3, the vertical axis is the most sensitive. When evaluating position 4, it has been obtained a value identical to the previous one. If the PO3V and POS4V points
are compared, it can be seen how it is in this latter position where the effect of the FTF frequency is greater, both in maximum accumulated values and in peak values, see Table 3.

In the case of position 4, the vertical axis is the most important, followed by the axial and finally the horizontal axis. When comparing both positions, it can be seen how the axial and vertical axes are the most important, but in absolute terms POS4V that is the most decisive. Table 4 shows everything.

The variable generated by the bearing balls follows a common pattern in positions 3 axial and 4 vertical, even though they have different axes. The vertical axis of position 4 is the highest. In terms of peak values, they are very equal in both positions.

The graphical analysis indicates that both positions are important and should be monitored, because it is not always the vertical axis that produces the highest peak value.

When this result is compared with that obtained by the BSF variable, it is determined that the peak value in the latter reaches 7.1 RMS. However, in the variable generated by the balls, the peak value of the vertical axis is 0.727 RMS, which is within the optimum working conditions. This indicates that this variable is not the cause of bearing failure or breakage. All this can be seen in Figure 4.

The BPOR analysis, in position 3, is the first variable where the most important effect is found in POS3H, its accumulated value is slightly higher than POS3V and both are very distant in relation to the axial axis.

| Table 3. FTF result in terms of RMS (mm/s) |
|-------------------------------|--------|--------|--------|--------|--------|
| Variable          | POS3H | POS3V | POS3A | POS4H | POS4V | POS4A |
| Total sum          | 52.480 | 55.880 | 51.590 | 94.970 | 9.480  | 59.040 |
| Average            | 0.090  | 0.080  | 0.100  | 0.170  | 0.159  | 0.110  |
| Peak value         | 0.520  | 1.340  | 0.560  | 7.610  | 7.747  | 1.180  |

| Table 4. BSF result in terms of RMS (mm/s) |
|-------------------------------|--------|--------|--------|--------|--------|
| Variable          | POS3H | POS3V | POS3A | POS4H | POS4V | POS4A |
| Total sum          | 29.246 | 38.188 | 47.724 | 41.482 | 56.812 | 48.113 |
| Average            | 0.048  | 0.062  | 0.078  | 0.068  | 0.093  | 0.089  |
| Peak value         | 0.573  | 0.672  | 0.692  | 0.933  | 0.727  | 0.627  |

In the analysis by values, the vertical axis of position 4 is the most important one to predict the failure of the frequency generated by the ball cage.

To fully validate the method, the FTF result on POS3 and POS4 is graphically compared to the vertical axis. The aim is to see if there is concordance and symmetry between the two, which allows us to state with complete certainty that the failure can be predicted, just analysing one of them.

Figure 3 shows that there is linearity between both and how it is in POS4V where the highest values are reached. This determines that it would be possible to predict the failure of this frequency, analysing only one of the six sampling positions.

It is important to highlight the ski curve effect, going from perfect operation values to breakage values higher than 7.1 RMS on days.

Once the FTF has been evaluated, BSF is analysed, starting from the third position and its axes, where the highest accumulated value and peak is obtained, which would be on the axial axis, with 47.7 RMS and 0.692 RMS, respectively. It has been obtained more incidence in the axial axis than in the vertical one, this indicates that position 3 is more sensitive to the vibration effect of this variable.

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Peak values are the same as cumulative values. It should be noted that these do not reach the risk values, as determined by the applied standard.

In position 4, the most sensitive axes are the horizontal and the axial, both in peak values and in accumulated values. It should be noted that in position 3 the values do not reach the risk values for the machine’s operation.

The analysis of the BPOR frequency in accumulated values determines that POS3V is the most sensitive in position 3, and in the case of position 4, it is obtained in POS4A. The comparison of both determinates that position 4 is the most decisive. All the above is shown in Table 5.

Table 5. BPOR result in terms of RMS (mm/s)

<table>
<thead>
<tr>
<th>Variable</th>
<th>POS3H</th>
<th>POS3V</th>
<th>POS3A</th>
<th>POS4H</th>
<th>POS4V</th>
<th>POS4A</th>
</tr>
</thead>
<tbody>
<tr>
<td>Average</td>
<td>0.032</td>
<td>0.027</td>
<td>0.017</td>
<td>0.034</td>
<td>0.027</td>
<td>0.053</td>
</tr>
<tr>
<td>Peak value</td>
<td>0.346</td>
<td>0.213</td>
<td>0.099</td>
<td>0.307</td>
<td>0.272</td>
<td>0.411</td>
</tr>
</tbody>
</table>

The variable generated by the balls in the outer track of the bearing follows a common pattern in POS3H and POS4A positions, even though they have different axes. When comparing the graph, it has been obtained linearity between both positions and axes, this determines that the most severe action is the one perceived by POS4A, as shown in Figure 5.

The study of the BPIR variable on axis 3 determines that the most sensitive axis in cumulative values and peaks is the axial, followed by the vertical position. In the case of position 4, it has been obtained that the most important axis is the horizontal one, followed at great distance by the vertical one.

It should be noted that the effect between the axial and vertical axes of position 3 is closer, in cumulative terms, than those obtained between the horizontal and vertical axes of position 4.

Fig. 5. BPOR result in terms of RMS(mm/s) at positions 3 horizontal and 4 axial

The analysis of the peak values determines that the axes 3 axial and 4 horizontal are the most important, but these do not reach values higher than 0.6 RMS, well below the critical 7.1, established by the existing legislation.

When comparing both positions, the result is that the axial position 3 is the one that perceives most the vibration effect of this variable, followed very closely by the horizontal position 4, with a little more than 1 RMS of difference. The same result is obtained in terms of peak values. Table 6 shows everything.

The variable generated by the balls in the inner track of the bearing follows a common pattern in POS3A and POS4H positions, even though they have different axes. This result is important because the linearity between both control points and determines that monitoring is possible by observing either of them, as shown in Figure 6. The study of the variable 2BSF on the 3rd axis determines that the most sensitive axis in cumulative values and peaks is the vertical one, followed by the horizontal position. In the case of position 4, the most important axis is the horizontal one, followed at great distance by the vertical one.

In position 4, the highest value is obtained on the horizontal axis, followed at a great distance by the vertical and axial axis. It should be noted that the effect between the horizontal and vertical axes of position 3 and 4 is very close in cumulative terms. The analysis of the peak values determines that axis 3 vertical and 4 horizontal are the most important. These values do not exceed 1.6 RMS, being well below the critical value of 7.1 RMS.

When comparing both positions, It has been obtained that the vertical position 3 is the one that most perceives the vibration effect of this variable, followed very closely by horizontal position 4, with little more than 2 RMS difference. In terms of peak values, It has been obtained the same result (see Table 7).

Table 6. BPIR result in terms of RMS (mm/s)

<table>
<thead>
<tr>
<th>Variable</th>
<th>POS3H</th>
<th>POS3V</th>
<th>POS3A</th>
<th>POS4H</th>
<th>POS4V</th>
<th>POS4A</th>
</tr>
</thead>
<tbody>
<tr>
<td>Total sum</td>
<td>36.364</td>
<td>42.149</td>
<td>52.048</td>
<td>51.198</td>
<td>29.070</td>
<td>18.113</td>
</tr>
<tr>
<td>Average</td>
<td>0.059</td>
<td>0.069</td>
<td>0.085</td>
<td>0.084</td>
<td>0.052</td>
<td>0.034</td>
</tr>
<tr>
<td>Peak value</td>
<td>0.456</td>
<td>0.542</td>
<td>0.593</td>
<td>0.482</td>
<td>0.426</td>
<td>0.147</td>
</tr>
</tbody>
</table>

Fig. 6. BPIR result in terms of RMS (mm/s) at positions 3 axial and 4 horizontal

The variable generated by the second harmonic of the balls follows a common pattern in positions POS3V and POS4H, even though they have different axes. This result is important and gives confidence to determine that it is possible to monitor the machine, observing the vertical position 3, as shown in Figure 7.

After evaluating the bearing frequencies, it is observed that the most determining variable is that produced by the second ball harmonic, followed by that of the cages.

The analysis of the peak values gives a more important result, obtaining in FTF 7.74 RMS a critical value of operation, making this frequency the most determinant, as shown in table number 8.

After identifying that the FTF is the most determining frequency of the SKFNU322 bearing, it is then compared with the results of the other two machine operating variables, such as SPEED and Blades.
Other studies determine that the turning variable of the machine generates more incidence in POS4V. In the case of the blades, the axial position would be the most important [2, 3]. In the Table 9 shows the comparison of the three frequencies.

The graph above shows the result of SPEED, Blades and FTF, with no linearity. It is certain that this machine can be monitored through positions POS4V and POS3A, as shown in Figure 8.

4. Conclusions

After the analysis of the variables FTF, BSF, BPOR, BPIR and 2BSF of the bearing SKFNU322, using the approximation method by power density values in accumulated values and peaks, it can be said that most important values are found in position 4, and specifically in the vertical axis.

In cumulative values, the actions created by 2BSF are the most important. However, in peak values, the most remarkable action is the one caused by FTF, with values higher than the critical ones, according to the application standard.

When comparing the FTF variable with the most representative of the machine, SPEED and Blades, it can be seen that the turning variable of the machine generates more effect in the vertical position, and the one on the blades has more effect in the axial position.

Finally, it can be concluded that despite studying 42 variables in six control points, it is possible to predict the failure of the bearing and avoid the stoppage of this equipment just monitoring POS4V and the SPEED variable.

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References


